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# Features of the synthesis of calcium-aluminate phases with the introduction of modifying additives

Một số đặc điểm về tổng hợp các pha canxi-nhôm sử dụng các phụ gia biến tính

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## Abstract

In this work, the influences of boric acid and high alumina cement used as modifying additives on the formation of  $CaO \cdot Al_2O_3$  and  $CaO \cdot 2Al_2O_3$  were studied. Herein, commercially available chalk of the M-90 label and technical alumina of the G-0 label were utilized as initial raw materials. Heat treatment of powder mixtures with various concentrations of modifying additives was carried out in the temperature range of 1250-1350°C with an isothermal exposure times of 1h and 2h. It was found that the addition of additives into the raw mixture affected the ratio of target phases and the temperature interval of the phase formation of calcium-aluminate minerals.

Keywords: Calcium-aluminate phases; heat treatment; boric acid; high alumina cement; modification.

### Tóm tắt

Trong nghiên cứu này, ảnh hưởng của các chất phụ gia như axit boric và xi măng alumin cao đến sự hình thành các pha CaO.Al<sub>2</sub>O<sub>3</sub> và CaO.2Al<sub>2</sub>O<sub>3</sub> đã được khảo sát. Trong đó, phấn thương mại M-90 và alumin kỹ thuật G-0 được sử dụng làm nguyên liệu ban đầu. Quá trình xử lý nhiệt hỗn hợp bột với các nồng độ phụ gia khác nhau được thực hiện trong khoảng nhiệt độ 1250-1350°C với thời gian nung là 1 và 2 giờ. Kết quả cho thấy rằng việc bổ sung các chất phụ gia vào hỗn hợp nguyên liệu thô ban đầu đã ảnh hưởng đến tỷ lệ pha của sản phẩm và khoảng nhiệt độ của giai đoạn hình thành khoáng chất canxi-aluminat.

*Từ khóa:* Pha canxi-aluminat; xử lý nhiệt; axit boric; xi măng alumin cao; biến tính.

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# **1. Introduction**

CaO·Al<sub>2</sub>O<sub>3</sub> (CA) and CaO·2Al<sub>2</sub>O<sub>3</sub> (CA<sub>2</sub>) are the main phases of calcium aluminate cement, which are widely used in the construction, mining and metallurgical industries [1] and are also considered as promising biomaterials, especially in dentistry and orthopedics [2]. Cement with an aluminum oxide content of more than 70 wt. % are called high alumina cement (HAC). The main ways of producing HAC are complete melting of the raw mix and sintering. In these processes, clinker is produced mainly by solid-phase reactions [3-5]. Highly pure HAC is produced by sintering in rotary kilns (in case of multi-tonnage production) as well as in tunnel or chamber kilns (in medium-tonnage production) [6, 7].

The development of the composition and technology for producing highly pure HAC includes: (i) the study of the synthesis process of clinker minerals; (ii) the identification of factors that determine the conditions of formation and temperature ranges of the target

 Table 1. Chemical composition of raw materials

phase CA and CA<sub>2</sub>; and (iii) the definition of technological and physical-mechanical characteristics of the finished product [8-13].

The aim of this work was to investigate the effect of some modifying additives on the phase formation processes of CA and CA<sub>2</sub> in the production of high alumina clinker.

#### 2. Methodology

When calculating the content of raw materials in the charge, it was assumed that high alumina clinker with 71-72 wt. % of Al<sub>2</sub>O<sub>3</sub> and 27-28 wt. % of CaO would be produced. This mass ratio in the CaO - Al system state diagram suggests the presence of two calciumaluminate phases CA and CA<sub>2</sub> [14, 15]. The predicted phase composition of the clinker is 64 wt. % CA and 36 wt. % CA2. Chalk of M-90 and technical alumina of G-0 labels were used initial raw materials. The chemical as composition of the feedstock is shown in Table 1. A more detailed description of the starting materials can be found in [16].

Material from	wt. (%)								
	Al <sub>2</sub> O <sub>3</sub>	SiO <sub>2</sub>	Fe <sub>2</sub> O <sub>3</sub>	CaO	MgO	Na <sub>2</sub> O	Other		
G-0	98.60	0.02	0.015	tracks	tracks	0.10	1.26		
M-90	0.10	0.10	0.08	98.60 (Ca	aCO <sub>3</sub> ) tracks	tracks	1.12		

As is known, initiators for the formation of new phases can be introduced in limited quantities of chemical substances close in nature as "seed". In our study, HAC (NK-CEM 72) with 70.50 wt. % Al<sub>2</sub>O<sub>3</sub> was the source of phase-forming initiator substances. In terms of mineralogical composition, HAC is represented by two phases: CA and CA<sub>2</sub>. The content of these phases is 78.5 and 21.5 wt. %, respectively.

One of the technological ways to reduce the operating temperature of phase formation is the introduction of additives that ensure the early emergence of micro-melts. This process intensifies the diffusion of cations and anions into the reaction zone. As an additive of this type, we chose boric acid of the chemically purified label.

The phase composition of materials was determined by X-ray diffraction analysis (XRD) conducted on an Ultima IV diffractometer (Rigaku Japan) using CuK $\alpha$  radiation ( $\lambda = 1.54056$  Å), Bragg-Brendano imaging scheme, with a scanning speed of 2 deg/min in the 2 $\theta$  angle range of 10-70° at 0.02° scanning steps. The peak identification was

performed using the PDF-2 database. Experimental diffractograms were processed using PDXL software (Rigaku Corporation) with Rietveld refinement. The phase ratio was calculated using the corundum number method.

The synthesis of clinker minerals was carried out as follows. Dosing of raw materials and modifying additives was carried out by the weight method on laboratory technical scales. The homogenization of the raw mix was performed by mixing in a drum of a laboratory ball mill with a working volume of 2L for 60 min. The prepared powder mixture was moistened with distilled water to a pasty state and homogenized with an overhead paddle mixer. The resulting mass was then placed in polypropylene molds with a diameter of 40 min and a height of ~ 30 mm, followed by vibration compaction for 10 - 20 seconds. The moulded samples were pre-conditioned at room temperature for 8h and then incubated in a forced convection drying oven at 120°C for 2h. The dried briquettes were placed in a Nabertherm LHT 02/17 high-temperature furnace on a corundum substrate and heated as follows: heating rate 250°C per hour, the first isothermal holding at 900°C for 30 min, the second isothermal holding at the given maximum temperatures for 1 or 2 hours.

# 3. Results and discussion

At the initial stage of the study, the effect of the addition of boric acid on the formation of the clinker phases was evaluated. For this purpose, the samples were prepared with the addition  $H_3BO_3$  in the initial mixture, equal to 0.5 and 1.0 wt. % according to the procedure mentioned above. The heat treatment was carried out at 1250, 1300 and 1350°C with isothermal exposure for 1 and 2h. The obtained samples were investigated by the XRD technology. The results of the influence of additive  $H_3BO_3$  in the initial charge on the phase formation processes are shown in Figures 1, 2 and Tables 2, 3.



Figure 1. XRD patterns of heat-treated samples with 0.5 wt.% H<sub>3</sub>BO<sub>3</sub>, isothermal exposure time of 1h (a) and 2h (b).



Figure 2. XRD diffractograms of the sample containing 1 wt. % H<sub>3</sub>BO<sub>3</sub> with isothermal exposure time of 1 hour at 1250°C

**Table 2.** Influence of heat treatment modes on the phase composition of samples with the addition of  $H_3BO_3 0.5\%$ 

Phases	Maximum temperature (°C)							
	12	250	13	00	1350			
	Isothermal exposure time (h)							
	1	2	1	2	1	2		
	wt (%)							
a-Al2O3	15.5	-	14.8	-	-	-		
C <sub>12</sub> A <sub>77</sub>	16.2	-	7.6	-	-	-		
CA	64.1	76.6	54.1	70.7	78.8	68.7		
CA <sub>2</sub>	13.5	24.4	14.1	29.3	21.2	31.3		

Table 3. Influence of heat treatment modes on the phase composition of samples with the addition of  $H_3BO_3 1.0\%$ 

Phases	Maximum temperature (°C)								
	12	.50	1300		1350				
	Isothermal exposure time (h)								
	1 2		1 2		1	2			
	wt. %								
СА	67.7	62.1	67.6	66.3	68.0	66.0			
CA <sub>2</sub>	32.3	27.9	32.4	33.7	32.0	34.0			

It can be seen from Figure 1a and Table 2, after heat treatment at 1250°C with isothermal soaking for 1h, the target phases CA and CA<sub>2</sub>,

as well as  $\alpha$ - Al<sub>2</sub>O<sub>3</sub> and the intermediate phase C<sub>12</sub>A<sub>77</sub> were detected. Increasing the temperature up to 1300°C did not lead to a

change in concentration of alpha aluminum oxide (~15 wt. %), while the content of phase  $C_{12}A_7$  reduced from 16 to 8 wt. %. At the same time, an increase of the isothermal exposure up to 2h allowed obtaining only two target phases – CA and CA<sub>2</sub>, regardless of the maximum firing temperature (Figure 1b and Table 2). In the case of firing at 1350°C, the contents of CA and CA<sub>2</sub> phases in the clinker were close to the design value.

The increase of  $H_3BO_3$  concentration in the initial charge up to 1.0 % made it possible to obtain samples with the designed ratio of CA and CA<sub>2</sub> already at 1250°C and the exposure time of 1 hour (Figure 2, Table 3). A further increase in temperature and duration of isothermal exposure did not lead to a change in the qualitative and quantitative phase composition.

In the next phase of research, the effect of the HAC additive on the synthesis of clinker phases was evaluated. The phase formation processes of CA and CA<sub>2</sub> from the CaCO<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub> powder mixtures with the addition of HAC 5% in the temperature range of 1250 -1450°C were previously studied [16]. According to the data obtained after heat treatment at 1300°C, the samples did not contain appreciate amounts of calcium oxide; but at the same time, there was a decrease in aluminum oxide content and formation of  $C_{12}A_7$ . It was shown that an increase of the heat treatment temperature in the range of 1300 -1350°C did not result in a significant change in the phase composition of the samples.



# 2-theta (degree)

Figure 3. XRD pattern of reference sample with isothermal exposure for 1h at 1350°C.

Considering the above information, in the present study, the heat treatment of powder mixtures with HAC additive of 5; 7.5 and 10 wt. % was carried out at 1350°C with exposure times of 1 and 2h, respectively. A reference

sample without HAC additive synthesized under the same conditions was used for comparison. The obtained materials were studied by X-ray diffraction analysis. Since all samples had a comparable phase composition, a powder X-ray diffractogram of the reference sample is shown in Figure 3 as an example, according to which the main components of the obtained clinkers are the target phases CA and CA<sub>2</sub>, as well as  $\alpha$ - aluminum oxide and C<sub>12</sub>A<sub>7</sub>. The nature of the change in the phase composition of the samples at different concentrations of HAC in the experimental charge is shown in Table 4 and Figure 4.

Phases	Amount of additive (mass %)								
	Without a		5		7.5		10		
	suppler	nent							
	Isothermal exposure time (h)								
	1 2		1	2	1	2	1	2	
	wt, %								
a-Al2O3	32.6	12.7	17.4	15.3	9.1	-	7.2	4.0	
C12A77	35.2	66.6	60.1	57.5	62.5	75.1	68.5	62.8	
CA	27.1	13.7	17.3	21.2	21.5	22.2	20.2	17.2	
CA2	5.1	8.0	5.6	5.9	6.9	3.6	4.4	17.5	

Table 4	Effect of	HAC	additive	on a	clinker	content	after	firing at	1350°C
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As can be seen from Table 4, the addition of HAC had a significant effect on the change in aluminum oxide content during the 1-hour isothermal soak. The  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> content in the reference sample was 32.6%; and in the HAC concentration range of 5 – 10%, the aluminum

oxide content decreased from 17.4 to 7.2%. Correspondingly, the content of calcium monoaluminate increased from 35.2% (reference) to 60.1 - 68.5%. A similar pattern of change in  $\alpha$ -Al<sub>2</sub>O<sub>3</sub> was also observed when the isothermal exposure time was increased to 2h.



Figure 4. Dependence of total content of target clinker phases CA and CA<sub>2</sub> on HAC concentration; isothermal exposure time of 1h and 2h at 1350°C

Figure 4 shows that with an increase in the proportion of added HAC, there was also a

distinctive tendency to an increase in the total content of the largest phases CA and CA<sub>2</sub> at an

isothermal exposure time of 1h. In case of an increase in the duration of heat treatment up to 2h, the similar dependence was absent. At the same time, an extremum of total CA and CA<sub>2</sub> fraction was recorded, corresponding to HAC content of 7.5%.

## 4. Conclusions

It has been established that with the introduction of 0.5% H<sub>3</sub>BO<sub>3</sub> into the charge, the design parity of CA and CA<sub>2</sub> phases was reached after heat treatment at 1350°C for 2h. An increase in the content of the boric acid content to 1.0% allowed obtaining clinker phase composition to the designed one at 1250°C and the exposure time of 1h. A further in processing temperature increase and exposure time did not lead to a change in the qualitative and quantitative phase composition of high alumina clinker. It was shown that the introduction of HAC additive into the charge affected the quantitative phase composition of the investigated products. The correlation was found between the amount of added HAC and the reduction of unreacted  $\alpha$ -aluminum oxide content in the samples heat-treated at 1350°C for 1h. The total content of the target phases CA and CA<sub>2</sub> tended to increase with an increasing proportion of the added HAC. The maximum of the total fraction of CA and CA<sub>2</sub> was recorded as increasing the heat treatment duration up to 2h.

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#### References

- Kuznetsova T.V., Tabaler J. (1988). Alumina cement. Moscow: Stroyizdat. 272 p.
- [2] Parreira R.M., Andrade T.L., Luz A.P. et al. (2016). Calcium aluminate cement-based compositions for biomaterial applications. Ceram. Int. V. 42. P. 11732.
- [3] Margishvili A. P., Rusakova G.V., Gvozdeva I.A., Alexsev P. A., Kuznetsova O.S. (2008). New Nikoand Ultra-Low-Cement Refractory Concretes of JSC "Borovichi Refractories Plant" for Metallurgy and Glass Industry. New Refractories. №3. P. 121-126.
- [4] Ilyakin A.V., Baranov P. A., Pospelova E.I., Amurzakov A.N. (2008). New generation of magnesia shotcrete masses of LLC "Magnezit Group". New Refractories. №7. P. 17.
- [5] Krivoborodov Yu., Samchenko S. (2019). Synthesis of high alumina cement based on metallurgy wastes. IOP Conf. Series: Materials Science and Engineering. Vol. 687. №2. P. 1 7.
- [6] Steennessen I., Boer A., Kockejei-Lorenz R. (2003). *High-purity high alumina cement; production and properties*. New Refractories. №8. – P. 22-27.
- [7] Migal' V.P., Skurikhin V.V., Gershkovich S.I. (2012). Production and Equipment Hign-Alumina Cembor Cements for Low-Cement Refractory Concretes. Refractories and Industrial Ceramics. Vol. 53. №1. P.4 - 8.
- [8] Zawrah M.F., Shehata A.B, Kishar E.A., Yamani R.N. (2011). Synthesis, hydration and sintering of calcium aluminate nanopowder for advanced applications. Comptes Rendus Chimie. Vol.14. № 6. P. 611 - 618.
- [9] Park Y.J., Kim Y.J. (2007) Effects of crystals structures on luminescent properties of Eu doped Ca-Al-O systems. J. Ceram. Int. P. 2843.
- [10] Hofmeister A.M., Wopenka B., Locock A.J. (2004) Spectroscopy and structure of hibonite, grossite, and CaAl2O4: Implications for astronomical environments. Geochimicaet Cosmochimica Acta. Vol. 68. № 21. P. 4485 - 4503.
- [11] Iftekhar S., Grins J., Svensson G.et al. (2008) Phase formation of CaAl<sub>2</sub>O<sub>4</sub> from CaCO<sub>3</sub>-Al<sub>2</sub>O<sub>3</sub> powder mixtures. Journal of the European Ceramic Society. Vol. 2. Pp. 747-756.

- [12] Rades S., Hodoroaba V.-D., Salge T., Wirth T., Lobera M.P., Labrador R.H., Natte K., Behnke T., Grossa T., Unger W. E. S. (2014) *High-resolution imaging with SEM/T-SEM, EDX and SAM as a combined methodical approach for morphological and elemental analyses of single engineered nanoparticles.* RSC Advances. Vol. 91. №4. P. 49577 - 49587.
- [13] Bhattacharyya S., Prasad B. (2013). Studies on phase formation in high alumina cement by varying manufacturing parameter and effect of those phases in refractory castable. Rourkela, 66 p.
- [14] Jerebtsov D.A., Mikhailov G.G. (2001). *Phase diagram of CaO-Al*<sub>2</sub>O<sub>3</sub> system. Ceramics International. №27. P. 25–28.
- [15] Hai-yan Yu, Yong-pan Tian, Xiaolin Pan, Gan-feng Tu. (2020) Mineral transition and formation mechanism of calcium aluminate compounds in CaO-Al<sub>2</sub>O<sub>3</sub>-Na<sub>2</sub>O system during high-temperature sintering. International Journal of Minerals Metallurgy and Materials. Vol. 27. №7. P. 925– 932.
- [16] Trubitsyn M.A., M.N. Yapryntsev, L.V. Furda, N.A. Volovicheva, V.I. Kuzin, R.V. Zubashchenko. (2022). Effect of heat treatment modes on process of synthesis of calcium-aluminate phases in the technology of high-purity high-alumina cement. Review of Belgorod State Technological University named after V.G. Shukhov. V.7, №2. – P. 84-93.